



Seeking minimum entropy production for flow-field patterns and geometries in fuel cells

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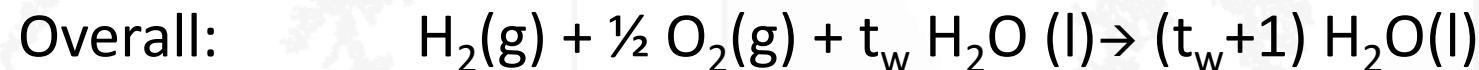
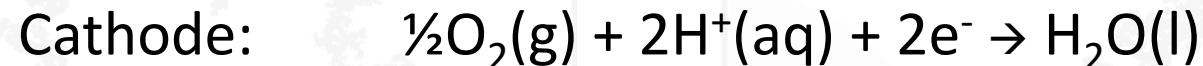
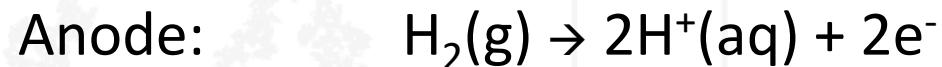
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Summary

- Aim:
 - Optimize tree-shaped flow field pattern for PEMFCs by minimizing the entropy production (EP).
 - Find design criteria
- Method:
 - 1D calculations using analytic pressure drop and EP in MATLAB
 - 3D simulations with OpenFoam's simpleFoam solver
- Results:
 - Larger width scaling parameters than the one from Murray's Law give lower entropy production
 - Channel width has the biggest influence on entropy production
 - Peclet number analysis gives range of current densities to use

PEM fuel cell

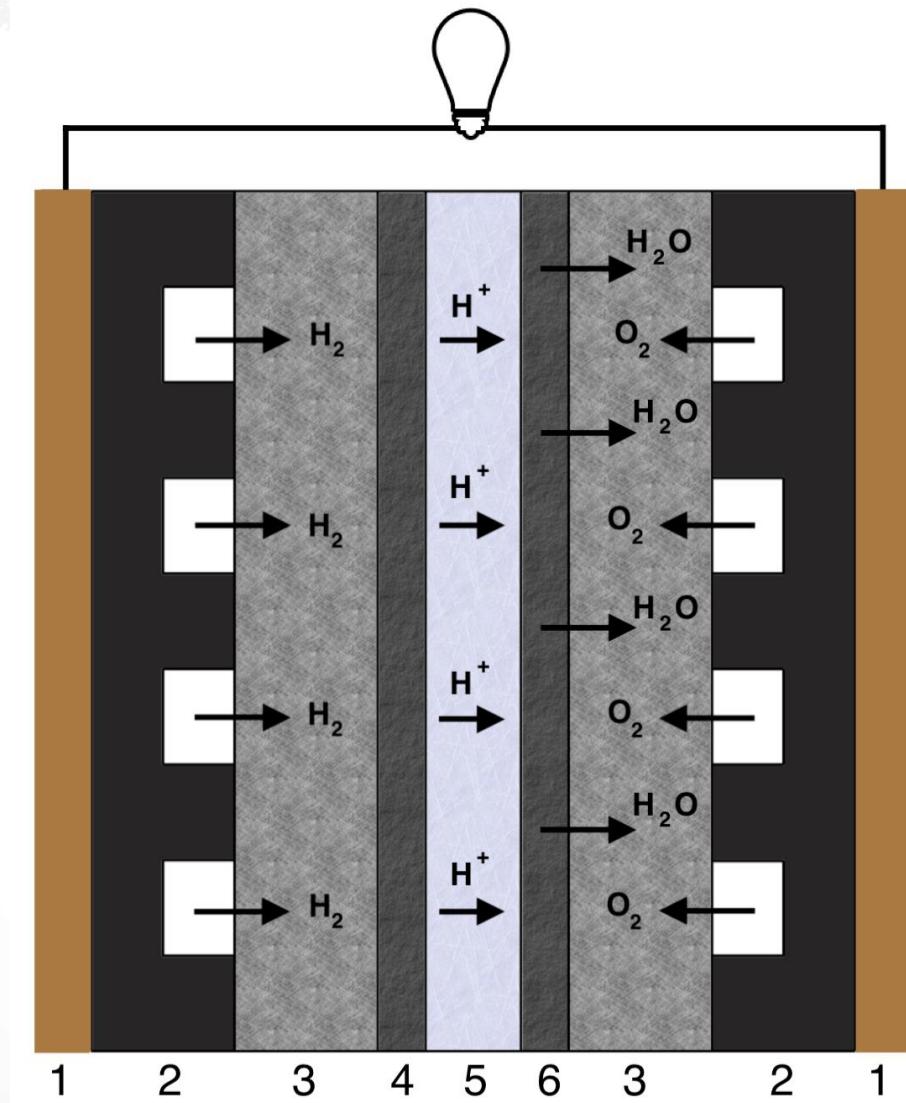
- PEM= Proton exchange membrane or polymer electrolyte membrane
- Core element: ion exchange membrane (mostly Nafion)
- Fuel: H₂ & O₂
- Exhaust: H₂O + excess gases





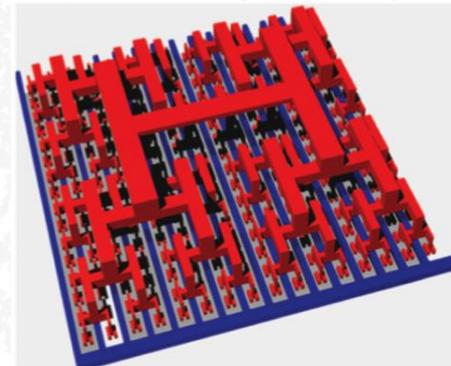
PEM fuel cell

- 1 – Current collector
- 2 – Flow field plate
- 3 – Gas diffusion layer (GDL)
- 4 – Anode
- 5 – Membrane
- 6 – Cathode

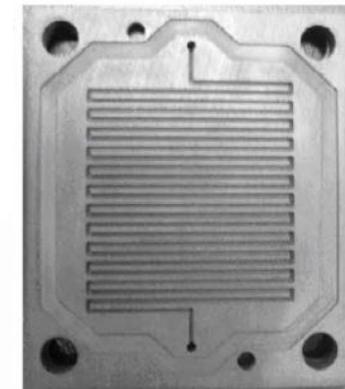


Introduction

- Tree-shaped patterns proven to increase performance of PEMFCs compared to serpentine patterns [1]
- Uniform outlet flow rate to achieve uniform fuel distribution
- Murray's Law for scaling should deliver minimum EP [2]
- One of the goal is to have $Pe < 1$ at the outlet



Tree-shaped FFP [1]



Serpentine FFP [3]

[1] P. Trogadas, J. I. S. Cho, T. P. Neville, J. Marquis, B. Wu, D. J. L. Brett, and M.-O. Coppens. A lung-inspired approach to scalable and robust fuel cell design. *Energy Environ. Sci.*, 11(1), 2017.

[2] S. Gheorghiu, S. Kjelstrup, P. Pfeifer and M.-O. Coppins. Is the lung an optimal gas exchanger? In: *Fractals in Biology and Medicine*, ed. G. A. Losa, D. Merlini, T. F. Nonnenmacher and E. R. Weibel, Birkhauser Basel, Basel, 2005, pp. 31–42.

[3] Hong Liu, Peiwen Li, Daniel Juarez-Robles, Kai Wang, and Abel Hernandez-Guerrero. Experimental Study and Comparison of Various Designs of Gas Flow Fields to PEM Fuel Cells and Cell Stack Performance. *Frontiers in Energy Research*, 2014.



Questions

- Questions:
 - Is Murray's law the most efficient scaling for FCs?
 - How does the width influence the entropy production?
 - How can you estimate the exact pressure drop in the most accurate way?
 - Can we define a design criterion based on the Peclet number?



1D tree-shaped flow field pattern

$$l_{j,i} = \frac{1}{2^{j/k}} l_0$$

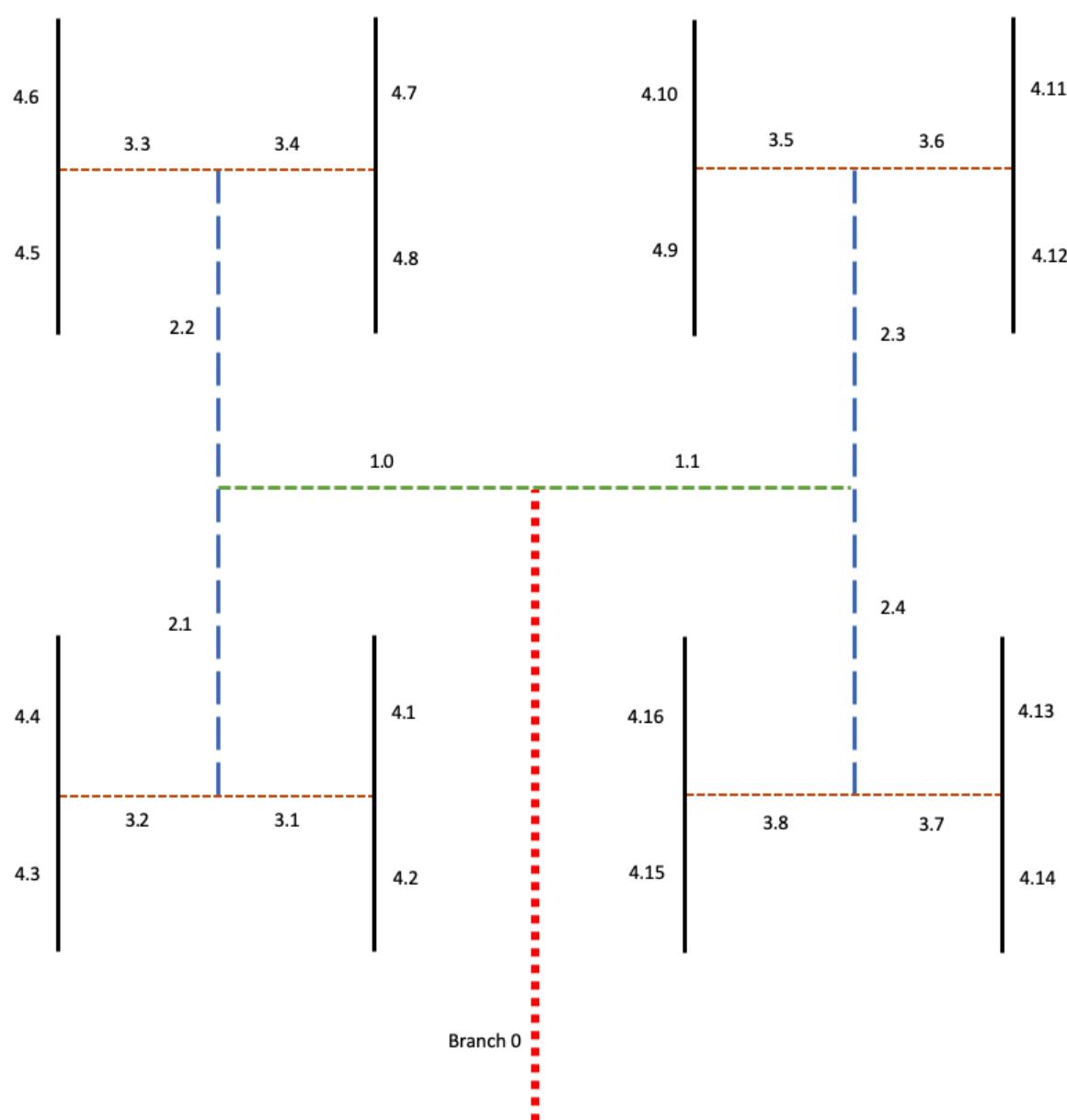
$$w_{j,i} = a^j w_0$$

$$Q_{j,i} = \frac{1}{2^j} Q_0$$

$$\left(\frac{dS_{irr}}{dt} \right)_{j,i} = -Q_{j,i} \frac{\Delta p_{j,i}}{T}$$

$$\frac{dS_{irr,spec.}}{dt} = \frac{dS_{irr}}{dt} w_{j,i}^{-1}$$

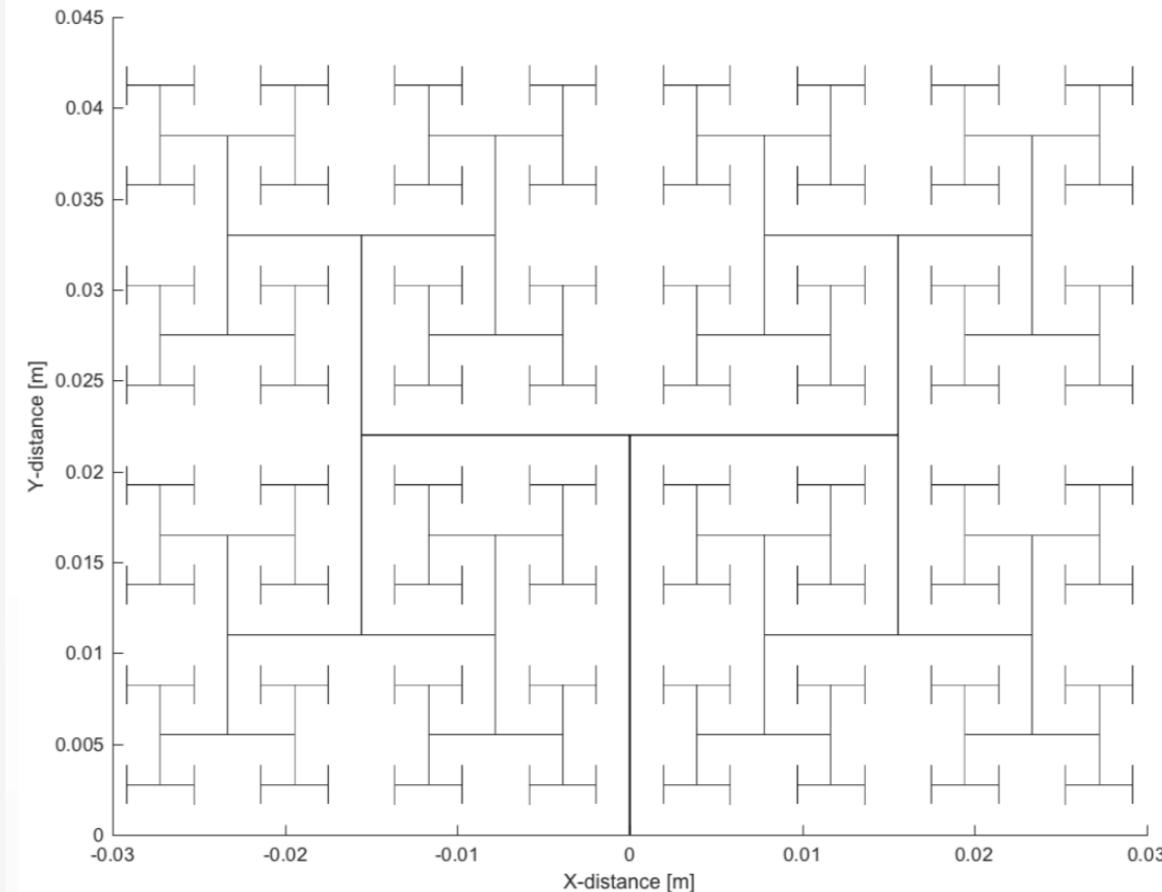
- Rectangular channels
- constant depth



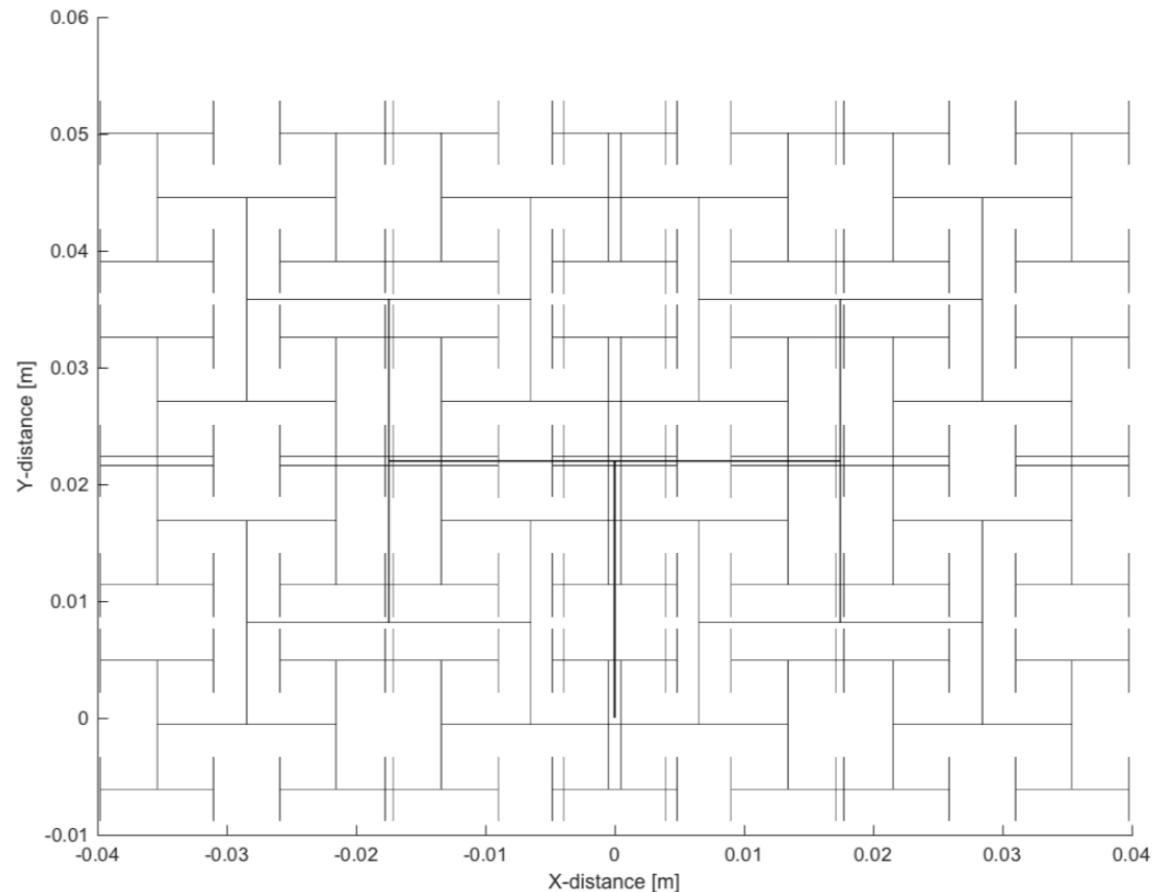


1D tree-shaped flow field pattern

$k=2$

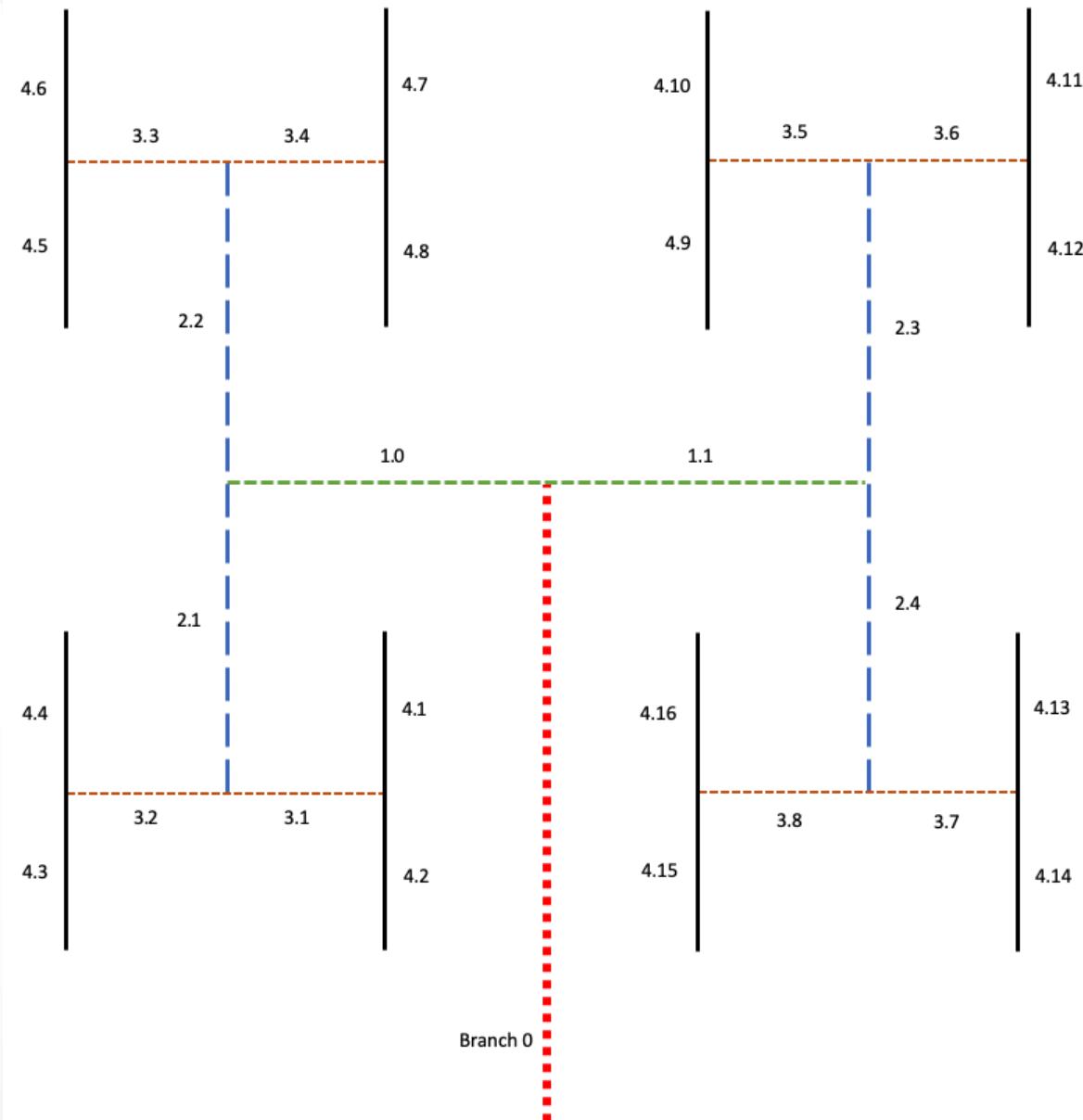


$k=3$



1D tree-shaped flow field pattern

- If lengths are scaled:
 - Rectangular area
 - Can have crossovers
- Therefore → no length scaling
- Space filling (25cm^2):
 - Gen. 0: $l=24\text{mm}$
 - Gen. 1: $l=12\text{mm}$
 - Gen. 2: $l=12\text{mm}$
 - Gen. 3: $l=6\text{mm}$
 - Gen. 4: $l=6\text{mm}$



1D – Pressure drop

$$\Delta p_{i,j} = -\frac{128\mu l_{i,j}}{\pi d_{i,j}^4} Q_{i,j}$$

- 3 different cases investigated

- Hydraulic diameter ($d_{j,i}=D_{j,i}$)

$$D_{j,i} = \frac{2w_{j,i}h_{j,i}}{w_{j,i} + h_{j,i}}$$

- Equivalent area

$$d_{j,i} = \sqrt{\frac{4}{\pi} w_{j,i} h_{j,i}}$$

- Analytic solution of HP-flow for rectangular channels

$$\Delta p_{j,i} = -Q_{j,i} \frac{12\mu l_{j,i}}{h_{j,i}^3 w_{j,i}} \left[1 - \sum_{n=0}^{\infty} \frac{192}{(2n+1)^5 \pi^5} \frac{h_{j,i}}{w_{j,i}} \tanh \left(\frac{2n+1}{2} \frac{\pi w_{j,i}}{h_{j,i}} \right) \right]^{-1} \quad [4]$$

[4] White, F. M. (2011). *Fluid Mechanics*. McGraw-Hill, 7 edition.



Case studies

Study	Investigation	Variables	Method
1	Flow rate & Δp calc. method dependency on TEP & TSEP	Flow rate, Δp calculation method, w_0	1D
2	Murray's Law and entropy production	a, w_0	1D
3	1D Δp	$a, \Delta p$ calculation method	1D
4	Flow rate distribution	a, w_0	3D
5	3D TEP & TSEP	a, w_0 , flow rate	3D
6	Comparison 1D & 3D Δp	$a, \Delta p$ calculation method, 3D pressure drop	3D, 1D
7	Peclet number	characteristic length, w_0, a , flow rate	1D

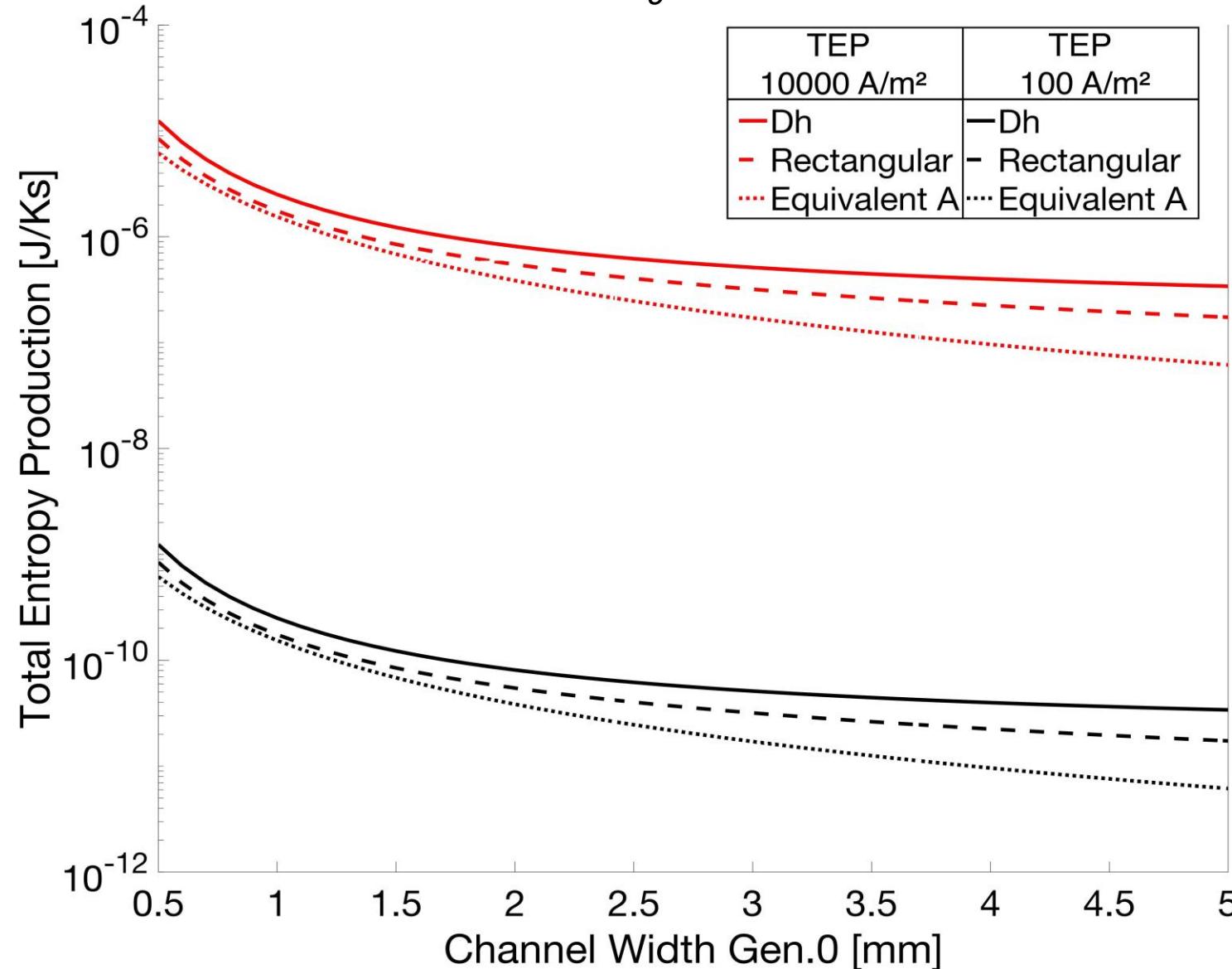


1D – Total entropy production results

Current density [A/m ²]	Flow rate [m ³ /s]
10000	5.7104×10^{-6}
5000	2.8552×10^{-6}
1000	5.7104×10^{-7}
100	5.7104×10^{-8}
10	5.7104×10^{-9}

$w_0=1\text{mm}$

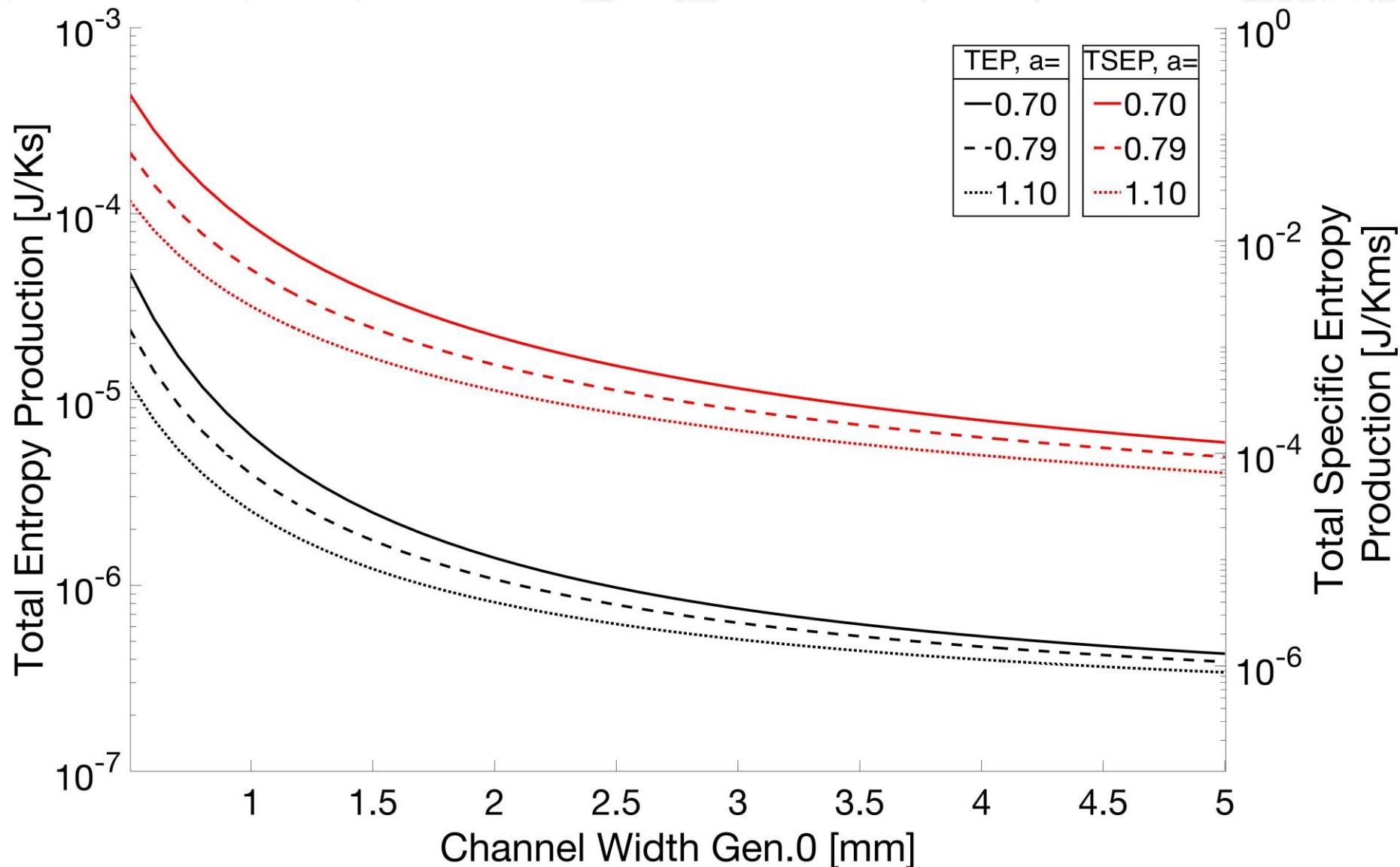
TEP	TEP
10000 A/m ²	100 A/m ²
Dh	Dh
Rectangular	Rectangular
Equivalent A	Equivalent A





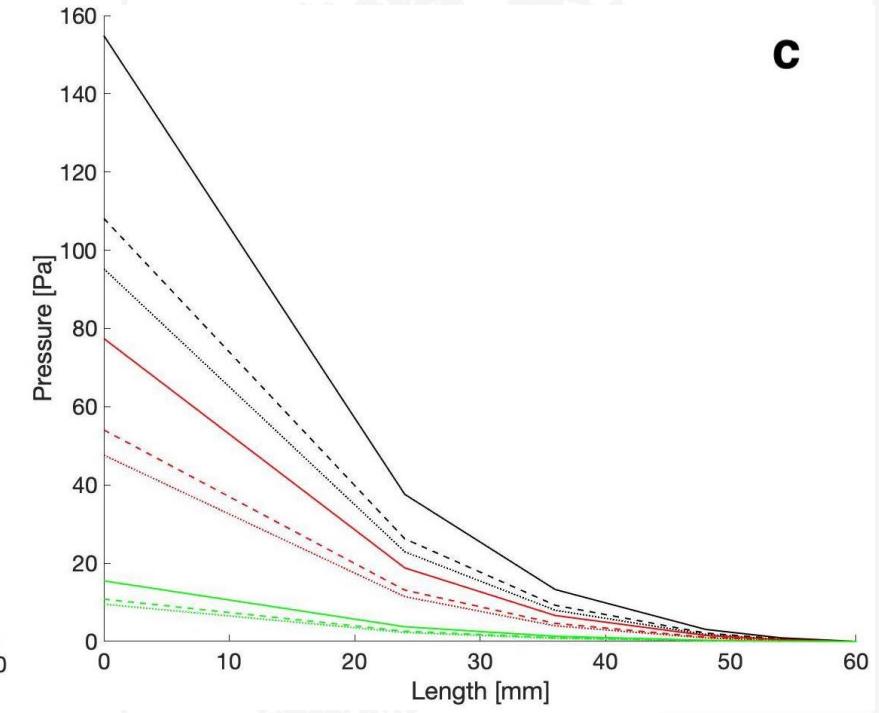
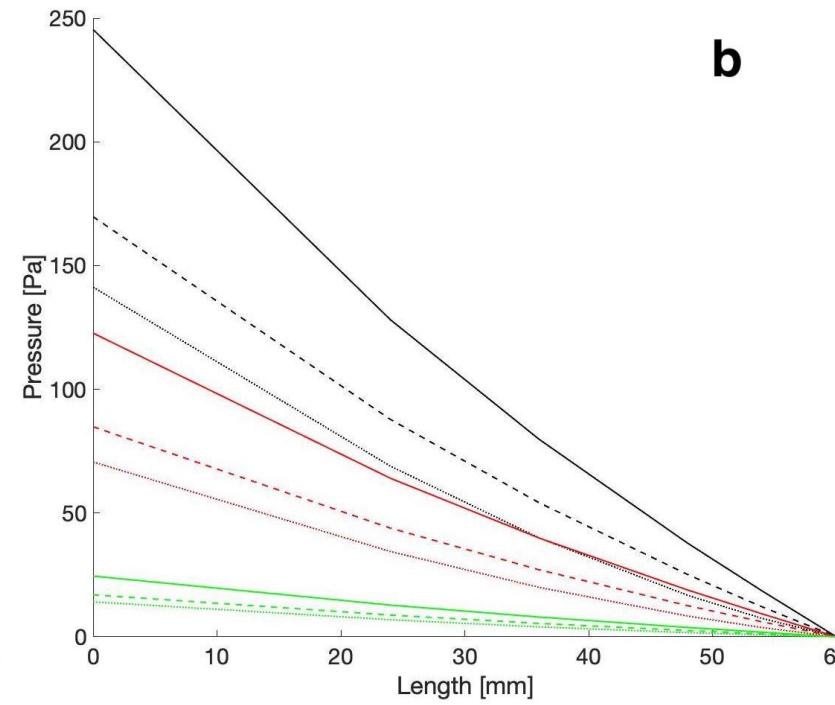
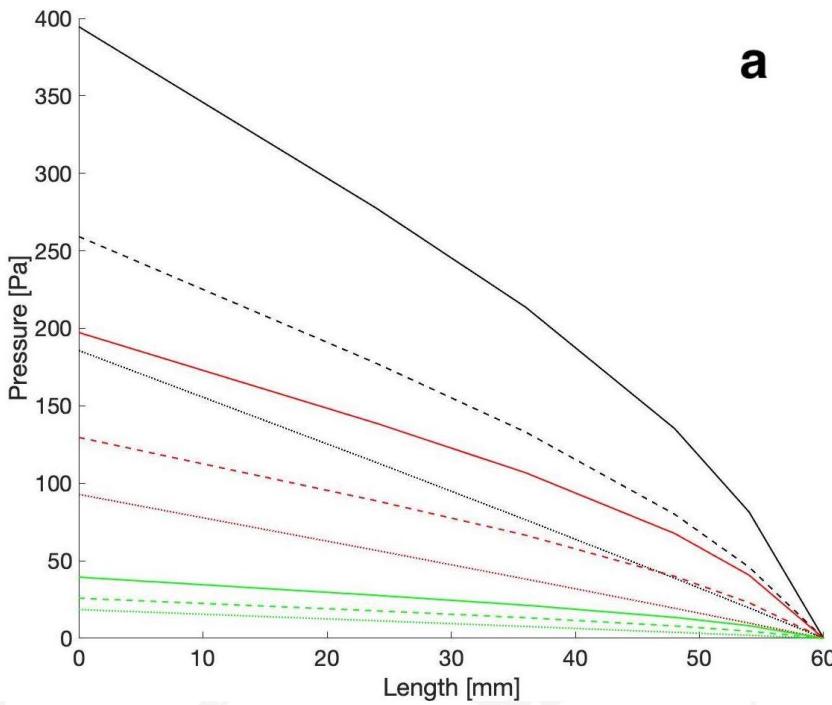
1D – Entropy production

$w_0=1\text{mm}$





1D – Pressure drop results



- a. $w_0=1\text{mm}$ $a=0.70$
- b. $w_0=1\text{mm}$ $a=0.79$
- c. $w_0=1\text{mm}$ $a=0.90$

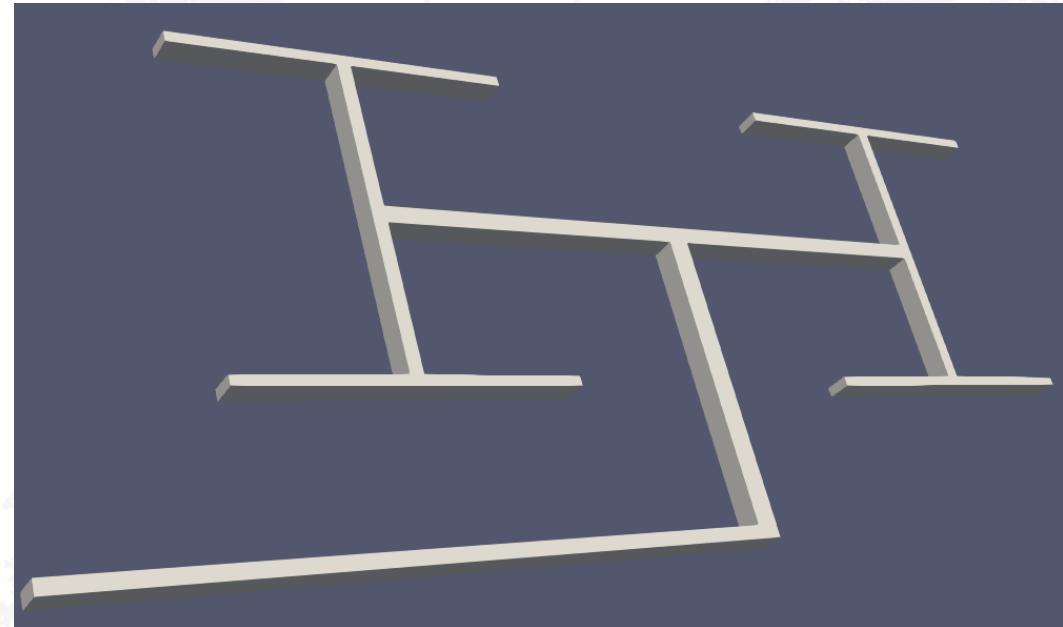
- Dh 10000 A/m²
- Rectangular 10000 A/m²
- Equivalent A 10000 A/m²
- Dh 5000 A/m²
- - Rectangular 5000 A/m²
- Equivalent A 5000 A/m²
- Dh 1000 A/m²
- - Rectangular 1000 A/m²
- Equivalent A 1000 A/m²

1D – Summary

- Flow rate shifts entropy production to higher or lower values
- Murray's law does not give lowest entropy production values
- Strong dependency on width from 0.5 to 2mm
- Form of pressure curve changes with a
- Reason for Murray's Law not being the optimum

3D – Simulation setup

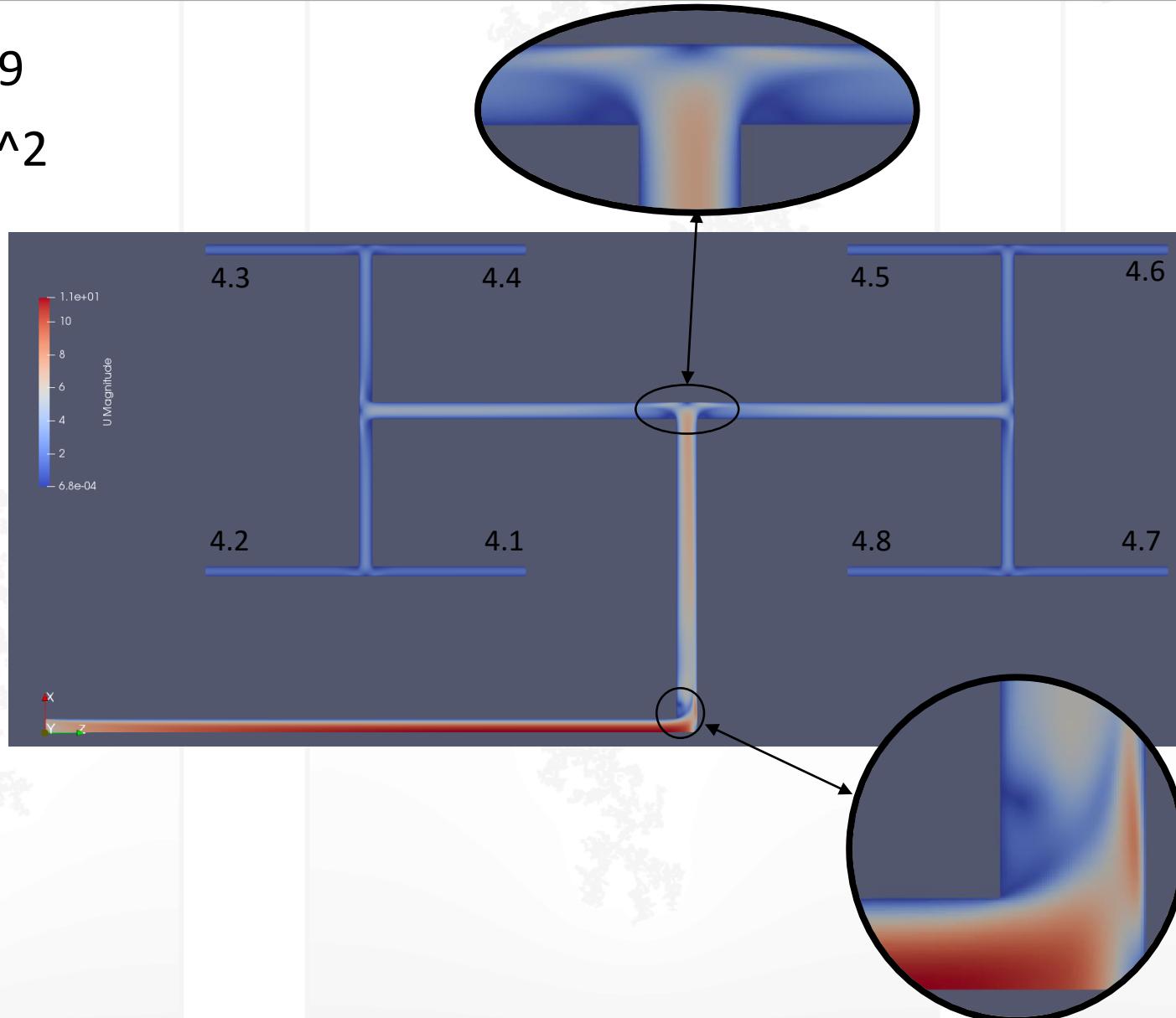
- Channel depth constant 1mm, channel width 1, 1.5, 2, 2.5 & 5mm
- α varied between 0.79, 0.9 and 1
- 4 generation levels
- Hexahedral mesh
- Incompressible, isothermal, laminar
- OpenFoam 4.1, simpleFoam





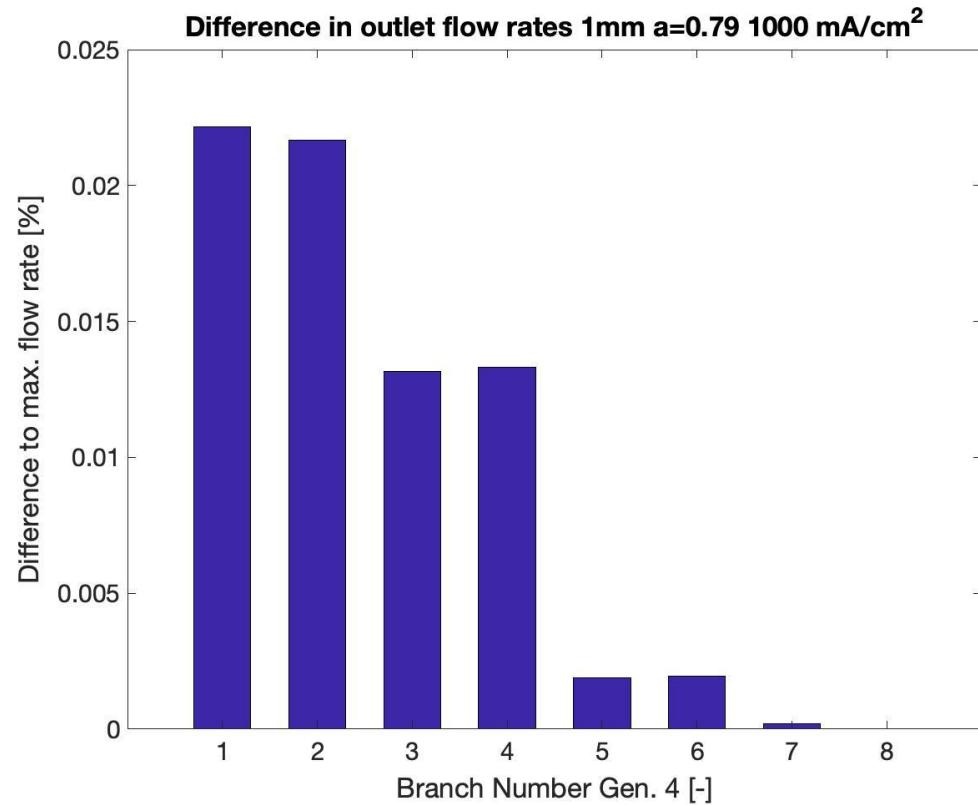
3D – Velocity & flow rate

- 1mm $a=0.79$
- 10000 A/m²





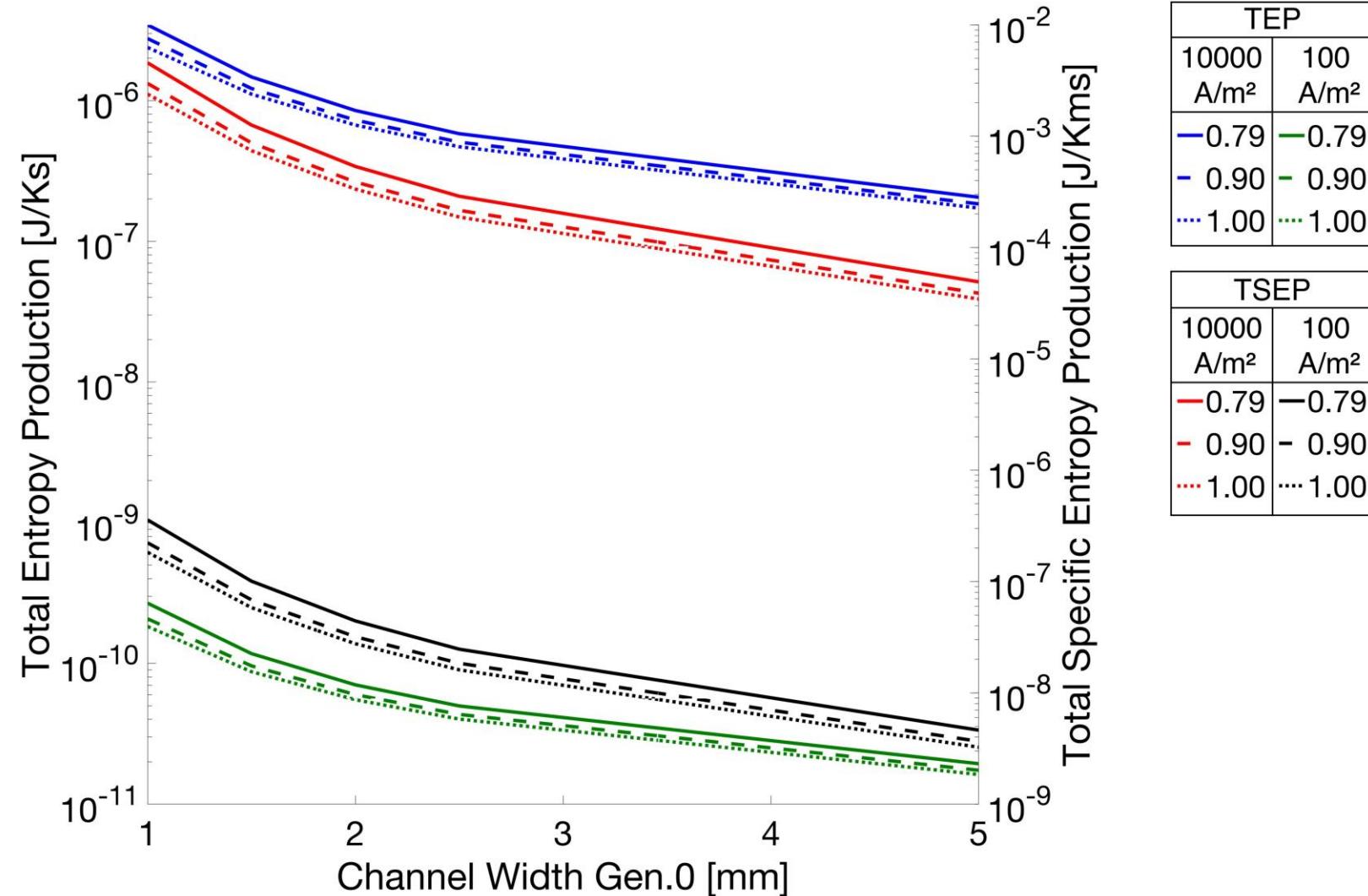
3D – Velocity & flow rate



	10000 A/m ²	5000 A/m ²	1000 A/m ²	100 A/m ²	10 A/m ²
$w_0 = 1\text{mm}, a = 0.79$	0.02	0.03	0.04	0.08	0.09
$w_0 = 1\text{mm}, a = 0.9$	0.11	0.20	0.27	0.53	0.56
$w_0 = 1\text{mm}, a = 1$	0.23	0.36	0.62	0.84	0.80
$w_0 = 1.5\text{mm}, a = 0.79$	0.03	0.01	0.01	0.01	0.01
$w_0 = 1.5\text{mm}, a = 0.9$	0.16	0.09	0.14	0.36	0.39
$w_0 = 1.5\text{mm}, a = 1$	0.37	0.14	0.17	0.46	0.47
$w_0 = 2\text{mm}, a = 0.79$	0.24	0.17	0.31	0.59	0.61
$w_0 = 2\text{mm}, a = 0.9$	0.29	0.03	0.04	0.09	0.09
$w_0 = 2\text{mm}, a = 1$	0.77	0.10	0.04	0.09	0.09
$w_0 = 2.5\text{mm}, a = 0.79$	0.20	0.02	0.03	0.06	0.07
$w_0 = 2.5\text{mm}, a = 0.9$	0.61	0.06	0.07	0.14	0.15
$w_0 = 2.5\text{mm}, a = 1$	0.75	0.11	0.18	0.34	0.37
$w_0 = 5\text{mm}, a = 0.79$	0.28	0.14	0.40	0.53	0.55
$w_0 = 5\text{mm}, a = 0.9$	2.54	0.41	0.70	0.90	0.91
$w_0 = 5\text{mm}, a = 1$	3.78	3.82	7.77	8.53	8.62

3D – Specific entropy production

$$\left(\frac{dS_{irr,specific}}{dt} \right)_{j,i} = \left(\int_{V_{j,i}} -\frac{1}{T} \Pi : \nabla v dV \right) \frac{1}{w_{j,i}} \quad [5]$$

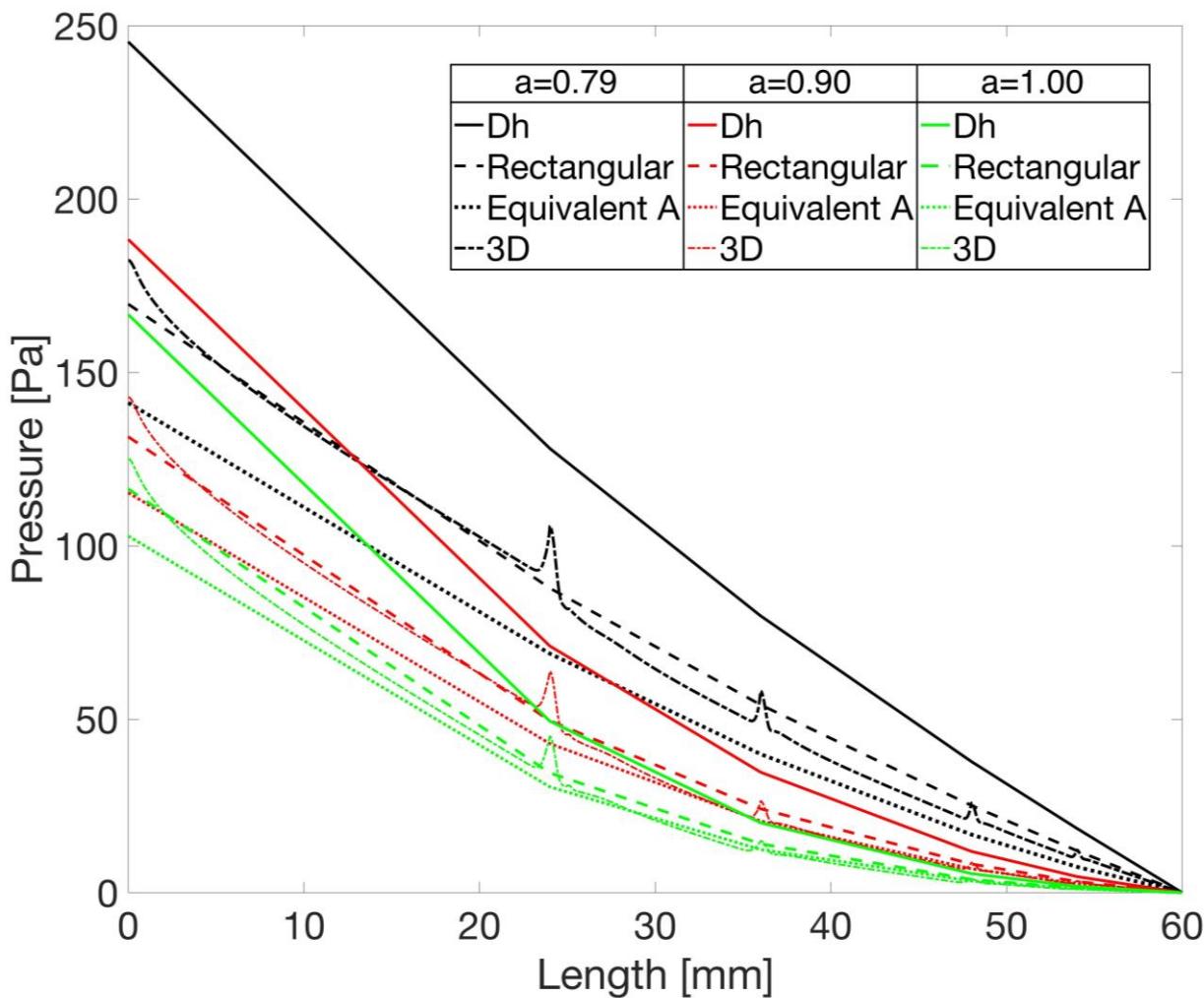


[5] S. Kjelstrup, D Bedeaux, E. Johannessen and J. Gross. Non-Equilibrium Thermodynamics for Engineers. World Scientific, 2 edition, 2017.

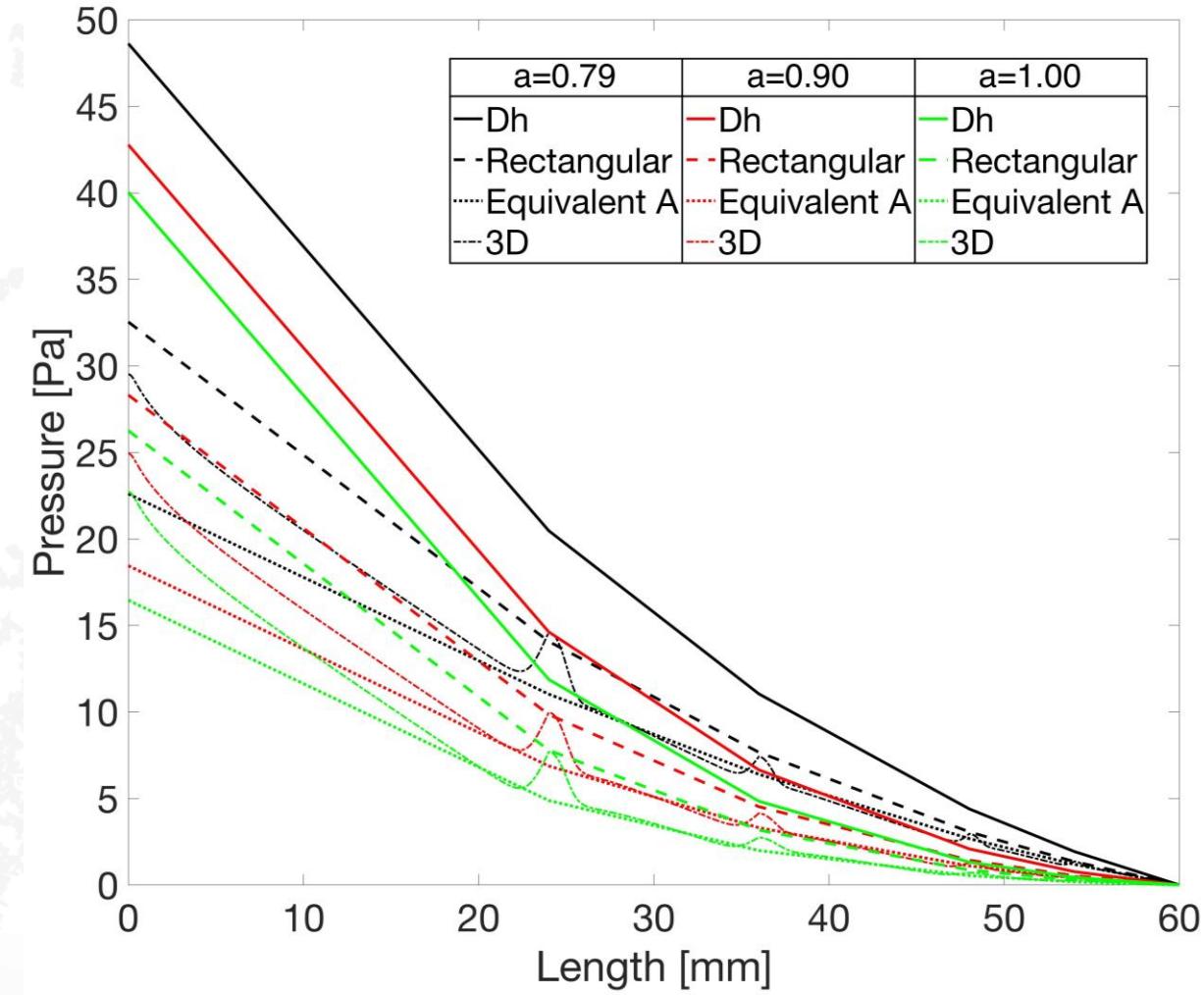


3D - Pressure

$w_0=1\text{mm}$



$w_0=2.5\text{mm}$



3D – Summary

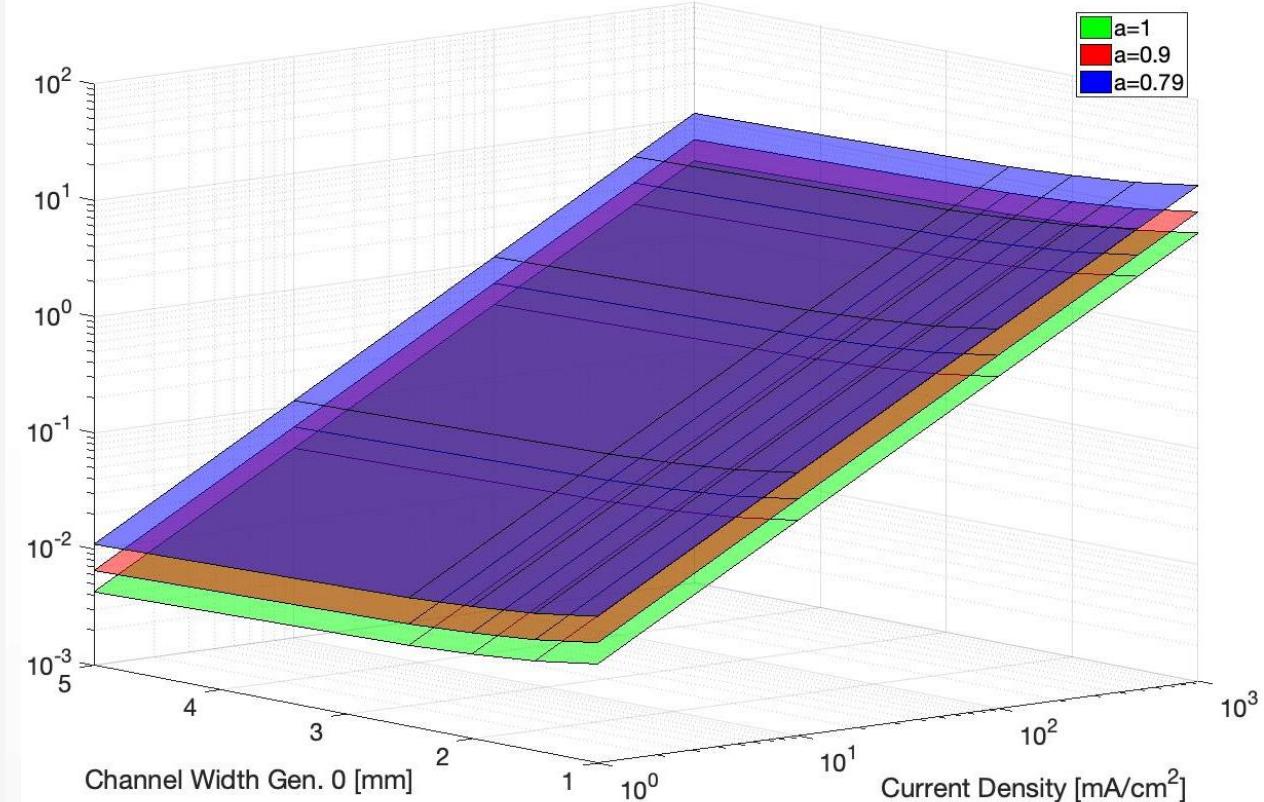
- Uniform flow distribution (beside $w_0=5\text{mm}$ cases)
- Results give same conclusions than for the 1D calculations
 - Murray's Law does not deliver the lowest entropy production
 - Increase in width → decrease in entropy production
- Most exact pressure drop calculation method depends on channel shape



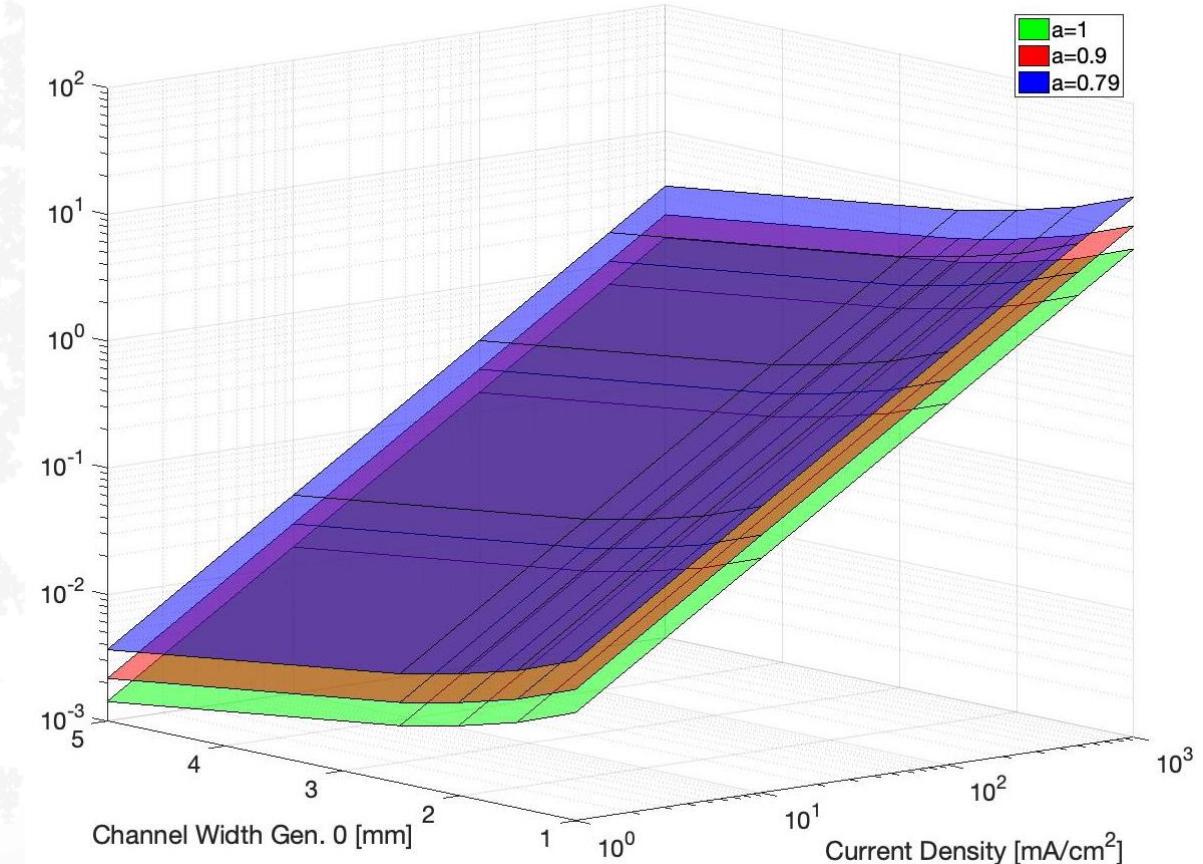
Peclet number

$$Pe = \frac{Lv}{D}$$

Peclet Number Gen. 4 $L=d_h$



Peclet Number Gen. 4 $L=w_4$



Discussion

- Due to uniform flow distribution, PEMFC can be subdivided
- Allows for approximation with 1D model
- Advantages of this pattern:
 - Easy to change space filling properties
 - Increase in generation levels does not increase pressure drop significantly ($a>0.79$)
 - This is due to the scaling
- Compared to serpentine:
 - Lower pressure drops achievable (1 order of magnitude) [6]
 - Uniform fuel distribution
- Not only applicable for PEMFCs, but also other fuel cells

[6] Su, A., Chiu, Y. C., and Weng, F. B. (2005). The impact of flow field pattern on concentration and performance in pemfc. *International Journal of Energy Research*, 29(5):409–425.

Conclusions

- Tree-shaped pattern provides uniform velocity/flow rate at end of last branches
- The higher the a , the lower the entropy production
- Scaling parameter a acc. to Murray's Law not optimal
- To use the hydraulic diameter approximation, overestimates the pressure drop and EP.
- The best way depends on the channel shape
- The Peclet number analysis gives a range of current densities where $Pe < 1$ can be achieved

Thank you for your attention!

Any questions?

Acknowledgements:

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