



• First used in textile engineering (Peirce, 1926)

• Statistical analysis (Daniels, 1945)

Different load-sharing rules:







3

A)

B)

C) Overloaded situation: applied load > critical load

- Loading by a fixed amount: expt. at lab
- Quasi-static loading: weakest link failure

**Different ways of Loading** 

 $\Box N'$ 



Х



# Problems in real-life















$$F(x) = N[1 - P(x)]\kappa .x$$

$$P(y) = \int_{0}^{y} p(x) dx$$

 $\boldsymbol{\sigma} = F(x) / N = [1 - P(x)] \kappa . x$ 





 $\circ$  F(x) has a maximum

• Put 
$$\frac{dF}{dx} = 0$$
  $1 - P(x_c) - x_c p(x_c) = 0$ 





**D**NTNU



 $D(\Delta) \propto \Delta^{-5/2}$ 

Hemmer & Hansen, 1992



 $N = 10^6; avg = 20000$ 

7





$$D(\Delta) \propto \Delta^{-5/2} (1 - e^{-\Delta/\Delta_c})$$
$$\Delta_c = \frac{1}{8(x_c - x_0)^2}$$



$$N = 10^6; avg = 50000$$

(Pradhan, Hemmer & Hansen; 2005)





.....onset of earthquake





 ${}_{\odot}$  The recursive dynamics

$$U_t = N_t / N$$

$$P(y) = \int_{0}^{y} p(x) dx$$

$$U_{t+1} = 1 - P(\sigma/U_t)$$

Uniform dist. 
$$U_{t+1} = 1 - \sigma / U_t$$

Fixed point 
$$U_{t+1} = U_t = U^* \longrightarrow U^{*2} - U^* + \sigma = 0$$

Solution 
$$U^*(\sigma) = \frac{1}{2} \pm (\sigma_c - \sigma)^{1/2}$$

(Pradhan, Bhattacharyya & Chakrabarti; 2001-02)





Order parameter

$$O = U^*(\sigma) - U^*(\sigma_c) \approx (\sigma_c - \sigma)^{1/2}$$

Susceptibility

$$\chi = \frac{dU^*(\sigma)}{d\sigma} \approx (\sigma_c - \sigma)^{-1/2}$$

Differential form

$$\frac{dU}{dt} = U_t - U_{t+1} = U_t - 1 + \frac{\sigma}{U_t}$$

**Relaxation time** 

$$au \propto \left( \sigma_{c} - \sigma 
ight)^{-1/2}$$

(Pradhan, Bhattacharyya & Chakrabarti; 2001-02)

#### Image: NTNU



 $t_f(\sigma)$  is the step/time to reach the fixed point



## Exact solution: Above critical stress

$$U_{t+1} = 1 - \frac{\sigma}{U_t} = 1 - \frac{\frac{1}{4} + \varepsilon}{U_t}$$

$$y_t = \tan v_t$$
  $\Box > 2\sqrt{\varepsilon} = \frac{\tan v_{t+1} - \tan v_t}{1 + \tan v_{t+1} \tan v_t} = \tan(v_{t+1} - v_t)$ 

$$v_t = v_0 + t \tan^{-1}(2\sqrt{\varepsilon})$$

solution

$$t_f(\sigma) = \frac{\pi}{2} (\sigma - \sigma_c)^{-1/2}$$

Pradhan & Hemmer 2006



PoreLab

NTNU-UiO Porous Media Laboratory



5-5-21

1

$$z_{t} = \tanh w_{t} \implies 2\sqrt{\varepsilon} = \frac{\tanh w_{t+1} - \tanh w_{t}}{1 - \tanh w_{t+1}} = \tanh(w_{t+1} - w_{t})$$

$$w_t = w_0 + t \tanh^{-1}(2\sqrt{\varepsilon})$$

solution

$$t_f(\sigma) = \frac{\ln(N)}{4} (\sigma_c - \sigma)^{-1/2}$$

Critical amp. ratio

$$\frac{\ln(N)}{2\pi}$$

Pradhan & Hemmer 2006







#### **Below critical stress**

#### Above critical stress



#### Pradhan & Hemmer 2006

15

Energy Budget of FBM



$$E^{e}(\Delta) = \frac{Nk}{2}\Delta^{2} (1-P(\Delta))$$

$$E^{d}(\Delta) = \frac{Nk}{2} \int_{0}^{\Delta} x^{2} p(\mathbf{x}) d\mathbf{x}$$









### $\frac{dE^e}{d\Delta}$ has a maximum in the stable phase







$$\Delta_c = G(\alpha) \Delta_{max}$$

 $\Delta_c = H(k) \Delta_{max}$ 



## Energy Budget: Signal of upcoming failure



# Test-case: Mixed-distribution









- Elastic energy growth rate shows a peak before collapse point.
- Signal of upcoming failure can be used to predict collapsesituations (rock failure, mine-collapse, borehole collapse ...)

- The energy framework will help to formulate a thermodynamic description of FBM
- o Can we calculate/check minimum entropy production principle?
- Collaborators: Alex Hansen, Per C. Hemmer, Jonas T. Kjellstadli, Bikas K. Chakrabarti





- Field theory for ELS dynamics (Hendrick, Pradhan, Hansen, PRE 2018)
- o RG scheme for ELS models (Pradhan, Ray, Hansen, Front. Phys. 2018)
- Energy budget in FBM (Pradhan, Kjellstadli, Hansen, Front. Phys. 2019)
- Stability issue in LLS models (Jonas, Eivind, .. Front. Phys. 2019)
- Fracture front propagation during fluid injection (Pradhan et al.)
- Stretching of biological systems (Eivind et. al.)
- Flow in a Fiber Tube Model (Roy, Sinha, Hansen, Front. Phys. 2019)

